Chemical Free Surface Processing of High Gradient Superconducting RF Cavities

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FMT Capabilities

• Founded in 1987, FM Technologies, Inc. (FMT) is a technology company with expertise in: charged particle beams, particle accelerators, plasma physics, electron/ion/microwave beam interaction with materials, microwave source development, pulsed power, and integration of these areas

• FMT has several projects approaching the commercial development stage:
  o Ceramic/Ceramic & Ceramic/Metal joining for use in high temperature chemical conversion processes
  o Self-Bunching Electron Guns with/without Current Amplification for Accelerators and RF sources
  o Microwave Plasma Torches for various applications
FMT Facilities/Equipment

- Headquartered in Chantilly, VA, FMT has over 10,000 ft² of available laboratory space and 8,300 ft² of available office space
- Offices equipped with advanced multi-core workstations loaded with a variety of sophisticated simulation and design software including:
  - EGUN, ICAP/SPICE, PARMELA, POISSON, SUPERFISH, SolidWorks, FEMM, HFSS, CSIRO, and FlexPDE-3D, FMT proprietary code FMTSEC (a 2 1/2D PIC code with secondary emission), MAGIC3D, CST, and an FMT 3-D relativistic particle pusher
- Laboratory has a full machine shop & plasma processing equipment:
  - Small and large (digital) precision lathes with high speed tool post grinder
  - 4-axis CNC milling machine
  - Digital milling machine
  - Grinding and sanding equipment
  - Acetylene, arc and spot welders
  - Cutoff saw
  - Band saw
  - Diamond saws
  - Small (digital) and large precision drill presses
  - Microwave assisted chemical vapor deposition system
  - RF and DC 3-gun sputtering system
  - 2773K brazing/joining furnace
FMT Facilities/Equipment

- Experimental hardware owned by FMT includes:
  - Pulsed Power Electron Beam and RF sources
    - Electron Beam System (1MV x 40kA x 0.1μs)
    - L-band (0.5 and 5 MW pulsed)
    - S-band (0.8, 1, 2.6 and 13 MW pulsed; 1 and 6 kW CW)
    - X-band (two 0.25 MW pulsed)
    - Broadband Amplifiers (50-2500 MHz, 50-100W CW)
  - MEIJI optical microscope w/ video out (400x, 2.5μm resolution)
  - Fast oscilloscopes
    - Ten 100-400MHz digital scopes
    - One 50GHz sampling scope
  - Particle transport magnetic coils
  - Cryo pump
  - Nine vac-ion pumps, 2-400 L/s
  - Six turbo molecular pumps, 60-400 L/s
  - Various roughing pumps
  - 1.5 MJ Capacitor bank
  - High-power RF components
    - Circulators
    - Isolators
    - Phase/amplitude adjusters
    - 0.1-1 MV pulse modulators
  - Chemicals, labware and glassware
  - Power supplies and other test equipment
Project Rationale and Approach

• SRF Cavity chemical treatment is expensive and complex
• After treatment surfaces still have numerous bubbles and pits
• Quench-producing weld defects and contamination result in significant scatter of Nb SRF cavity performance
• High costs and performance scatter are the major manufacturing problems
• FMT is developing an internal electron beam (IEB) system that will perform electron beam melting over the entire interior surface of Nb SRF cavities
• Result is a surface that is smooth without voids, bubbles, or imperfections
• This may allow manufacturing of the Nb SRF cavities with a reduction in chemical treatment and an increase in cavity high gradient performance
• FMT will design, build and test the new IEB system and process samples/cavities
• Thomas Jefferson Laboratory will measure RF performance of processed samples/cavities
Seven-Cell Nb SRF Cavity at Thomas Jefferson National Accelerator Facility

International Linear Collider alone needs 22,000 cavities at $210k (avg.) /cavity = $4.62 Billion
Typical SRF Cavity Defects
Pictures show typical defects inside Nb SRF cavities around the equator EBW overlaps that remain after chemical treatment:

- Irregularity (step) near equator at EBW overlap of cell and waveguide
- Two cells have less pronounced features; four cells have no recognizable features
- Many “bubbles” sporadically present inside the weld
- Many visible “deep pits” in heat affected zone
Objectives for Accelerator RF Cavity Processing

- Achieve a smooth surface with minimal defects and impurities to reduce quenching.
- Achieve a low strain surface to reduce corrosion and absorption of contaminants.
- Final goal is to attain *reproducible* high Q (>10^{10}) and high field (~40MV/m) cavities.
Electron Beam Melted Nb Samples Using J-lab SCIAKY Electron Beam Welder

Each single pass melt region is about 6 mm x 74 mm x 0.1-0.2 mm deep

A 10 kHz circular to elliptical raster with 0.5-1 mm beam diameter with a particle energy of 50 keV

Beam current and translation rates varied from 20-250 mA and 5-20 in/min

28 plates of Nb with dimensions 3 mm thick x 25.4 mm wide x 88.9 mm long
Magnification of Melt Zone

HIROX digital microscope view of sample #6

Bottom half of image shows the smooth melted region that highlights the grain size of about 300-400 µm, while upper half of image shows the rough un-melted small grain region.
Chemical Free Half-Cell Processed in J-lab’s SCIAKY E-beam Welder
Finished E-Beam Processed Half-Cell

The beam parameters were: 40 mA, 0.5mm diameter beam, travelling at 18 inches per minute, the melting diameter is about 6 mm with a circular pattern at 10 kHz.
Test and Prototype Evolution

Project is proceeding in three development phases:

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Stainless Steel Test Chamber

Chamber reaches $3 \times 10^{-8}$ Torr with test cathode, anode, high current and voltage feedthroughs.

Chamber hosted operational high voltage and current tests

Chamber suitable for time dependent magnetic fields with a diffusion time of $\sim 13$ ms

Turbo-pump

Cryo pump
Isolation Transformer

Purpose: to provide large AC current to heat the filament to provide a copious electron source for acceleration

Step-down transformer with primary and secondary coils without common grounding contained in an oil filed tank allowing the secondary to float to high voltage
Isolation (Filament) Transformer Design

- FMT design
- 2.3kVA, 115V RMS input
- 20A primary
- Capable of 430A @ 5.35V w/ 150kV isolation
- Tested to 330A and 100 kV.
Isolation Transformer Implementation

- Primary coil (from a dismantled variac)
- Secondary coil: 8 turns of #2 welding cable
- Turns ratio ~20
- Immersed in oil for high voltage operation
High Voltage (HV) Power Supply (PS)

Purpose: to provide a high voltage and power (50 kV, up to 15,000 watts) source to accelerate electrons

HV PS consists of:
- Variac
- HV Transformer
- Current Limiting Inductor(s)
- Full Wave Rectifier
- Filtering Capacitor(s)
- Output Resistor(s)
- Plastic Container Oil tank

HV PS must be resilient against short and open circuits suddenly and unexpectedly presented by the load. Circuit simulations aided these design goals.
HV PS Circuit Diagram and Simulations

Tested to $> 50$ kV and $> 40$ mA.
HV Power Supply Hardware Components

3uF, 100 kV capacitors to be connected in series

Full wave rectifier made from 36 20-kV diodes
100 Mohm resistors in parallel to equalize voltage across diodes

14 163-ohm resistors in series on PS output
HV Power Supply Hardware Components (cont.)

- Tank with rectifier, resistors, capacitors, and dummy load installed; oil being added
- Inductors wired in parallel with each other and in series with transformer
- Variac providing HV PS voltage control
High Voltage Transformer

- “E” core transformer
- 15kVA, 220V RMS input
- Four configurable secondary windings
- 2+2 configuration gives 230mA @ 65kV
Cathode/Anode Diode Assembly

Its purpose is to test beam generation at operational power within the chamber.

Cathode assembly is comprised of:

• Tantalum filament (Sciaky)
• Two Titanium mount/feeds
• Macor insulating block
• Aluminum feed-thru rods
Water-Cooled Target Assembly

Comprised of:

- Graphite Target
- Teflon Bushing
- Water-cooled Cu Heat Exchanger
- Shunt Resistor to measure current
Cathode/Anode Diode Assembly

Anode, Cathode, Filament, and Target in Chamber

Looking up inside and toward target

Filament in operation
Cathode-Anode System Test Setup

- Target Assembly
- Test Chamber
- Filament Current
- Bushing Feed Thru
- Isolation Transformer
- HV Bushing and Feed Thru
- HV Power Supply and connecting cable
Electron Gun and Ballistic Beam Transport Design Considerations

- Process from cell iris to equator and circumference
- Prevent Nb vapor arcing
- Tolerate beam induced thermal radiation & filament heat load

Electron Gun Characteristics:
- ~50 keV energy, up to 250 mA of current
- desire beam spot 0.5-1mm
- 10 kHz rastering capability
- gun diameter < cavity iris (~65 mm)
- long focal length (30-100 cm)
- current control independent of focus
Ballistic Focusing Gun

Pierce-like electrode provides 1st Focus, V adjustable -50 to -51kV with beam current unaffected

Anode, V=0

Cathode & Filament, V=-50kV

51mm Diameter

Two magnetic dipoles on x & y axes provide rastering, in circle or ellipse, V=0

Short “solenoid” w/Soft Iron Case: 2nd Focus, V=0

Magnetic & Radiative Heat Shield, Water Cooled, V=0

High Voltage Insulator
Ballistic Focusing Gun: Electron Beam Trajectory

Helmholtz coils provide R-Z beam scanning from iris to equator.

Azimuthal scanning provided by rotating the cavity about the Z axis in a fixed field provided by Helmholtz coils.
Electron Gun Implementation(s)

Two DC electron guns under development:

*Melt Effect Characterization Gun*

*Prototype DC Compact Electron Gun*
Prototype Compact DC Electron Gun (Design)

- 60 mm OD; overall length scalable.
- Uses SCI AKY Tantalum filament heated by AC current
- Designed for operation at 50 kV and 40 mA
- Beam focusing provided by Pierce electrode and downstream solenoid electromagnet
- Water cooled front face and solenoid magnet
Prototype Compact DC Electron Gun

SCIAKY Tantalum filament

Anode View

Cathode and Pierce Electrode View
Beam Melt Effect Characterization Gun

• Currently in production
• Consists of:
  – compact A-K assembly
  – compact focusing magnet and larger support assembly to allow for easier implementation of diagnostics while characterizing beam
• OD too large to fit inside of accelerator cavity
• Minimum beam diameter = 0.54 mm at target
• Larger radial gun size allows for easier assembly and diagnostics
• Explore parameter space properties to optimize performance:
  – electron energy
  – current
  – beam size
  – beam target beam spot locus speed and figure
Beam Melt Effect Characterization Gun

- anode
- cathode
- Pierce electrode
- Downstream solenoid focusing magnet not shown
Rotating Target Assembly

- Allows testing of a static electron beam (i.e. without steering magnetic field)
- Strips of test material (Nb, Cu, SS) are mounted on a rotating target disk
- Target strip is moved through fixed electron beam
- Target motion provided by an automatic digital indexing head and a rotary feedthrough (Ferrofluidic)
Rotating Target Assembly

- Base rests on bottom of vacuum chamber
- Connector on RHS of rod connects to programmable indexing motor
- Alumina rod connects to SS rod providing electrical isolation
- Received beam current is carried through SS rod and down isolated upright
- Four metal (e.g. Nb) strips are mounted on graphite target disk.
Rotating Target Assembly

Target front (graphite) with four copper strips installed

Automatic digital indexer: motor and controller connected to rotating target in vacuum chamber
Rotating Target Assembly

Downstream view showing current pickup, stainless steel to alumina rod joint, and rotating feedthrough

Upstream view of the back of the target in the beamline position
Summary and Status

• Beam parameters have been determined from real world tests that produce a smooth low strain Nb surface using a conventional rastered electron beam

• A step-down, Isolation Transformer was designed and built to provide the filament current and heating to provide sufficient thermal emission in the electron gun

• Stainless steel vacuum chamber hosted electron beam tests using HV supply, Isolation Transformer, custom anode and cathode at operational voltage and current

• HV power supply (up to 50 kV and up to 250 mA) has been constructed and tested

• A compact electron gun has been designed that is expected to produce a ballistic beam to meet the previously determined energy, current, and beam size requirements to process the surface of a Nb accelerator cell

• A second, larger electron gun with smaller beam diameter intended for beam melt characterization is in production and will begin testing within days

• A rotating target with mounting points for Nb strips and necessary x-ray shielding has been built to fit into and around the existing vacuum chamber and will accommodate various gun and target configurations.

• Follow-on goals: gun fabrication, gun driven melting of Nb strips, tests of the resulting surface quality, design and fabrication of a steering coil, and processing of a sample accelerator cell